



CR-343(11)

DIARY

82 0022

# Field Book

50% rag paper  
32 pages

4<sup>5</sup>/<sub>8</sub>" x 7<sup>1</sup>/<sub>4</sub>"

Keuffel & Esser Co., Morristown, N. J. 07960 Made in U.S.A.

CR-343(11) DIARY



### CURVE FORMULAS

$$T = R \tan \frac{1}{2} I$$

$$T = \frac{50 \tan \frac{1}{2} I}{\text{Sin. } \frac{1}{2} D}$$

$$\text{Sin. } \frac{1}{2} D = \frac{50}{R}$$

$$\text{Sin. } \frac{1}{2} D = \frac{50 \tan \frac{1}{2} I}{T}$$

$$R = T \cot. \frac{1}{2} I$$

$$R = \frac{50}{\text{Sin. } \frac{1}{2} D}$$

$$E = R \text{ ex. sec } \frac{1}{2} I$$

$$E = T \tan \frac{1}{4} I$$

$$\text{Chord def.} = \frac{\text{chord}^2}{R}$$

$$\text{No. chords} = \frac{I}{D}$$

$$\text{Tan. def.} = \frac{1}{2} \text{ chord def.}$$

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.) and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance. Multiply the angle by .01745, and the product by the distance.

### GENERAL DATA

RIGHT ANGLE TRIANGLES. Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt. 10.  $10^2 \div 200 = .5$ .  $100 + .5 = 100.5$  hyp.

Given Hyp. 100, Alt.  $25.25^2 \div 200 = 3.125$ .  $100 - 3.125 = 96.875 =$  Base.

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

LEVELING. The correction for curvature and refraction, in feet and decimals of feet is equal to  $0.574 d^2$ , where  $d$  is the distance in miles. The correction for curvature alone is closely,  $\frac{1}{2} d^2$ . The combined correction is negative.

PROBABLE ERROR. If  $d_1, d_2, d_3$ , etc. are the discrepancies of various results from the mean, and if  $\sum d^2$  = the sum of the squares of these differences and  $n$  = the number of observations, then the probable error of the mean =  $\pm 0.6745 \sqrt{\frac{\sum d^2}{n(n-1)}}$

### MINUTES IN DECIMALS OF A DEGREE

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

### INCHES IN DECIMALS OF A FOOT

1-16	3-32	$\frac{1}{8}$	3-16	$\frac{1}{4}$	5-16	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

PIPE HEAT NO.

REDUCER 36" 167091  
24" 611497  
ELBOW SW1312  
24" PIPE CH-1862380

APRIL 9, 1982

UTAH POWER AND LIGHT CREW  
CAME OUT AND MOVED THE POWER  
POLE BACK TO THE NEW R/W LINE.

Preston Ward



- HI A

639

525

362 52014

520476 548  
362

531

519920

548  
76

520463 345 519920

452

520117

520574 574 345

457

462

520000

520442  
534  
519928

574  
457  
117



BM'S TO SET PIPES NEAR THE  
INTERSECTION OF 10<sup>th</sup> WEST AND  
2ND NORTH.

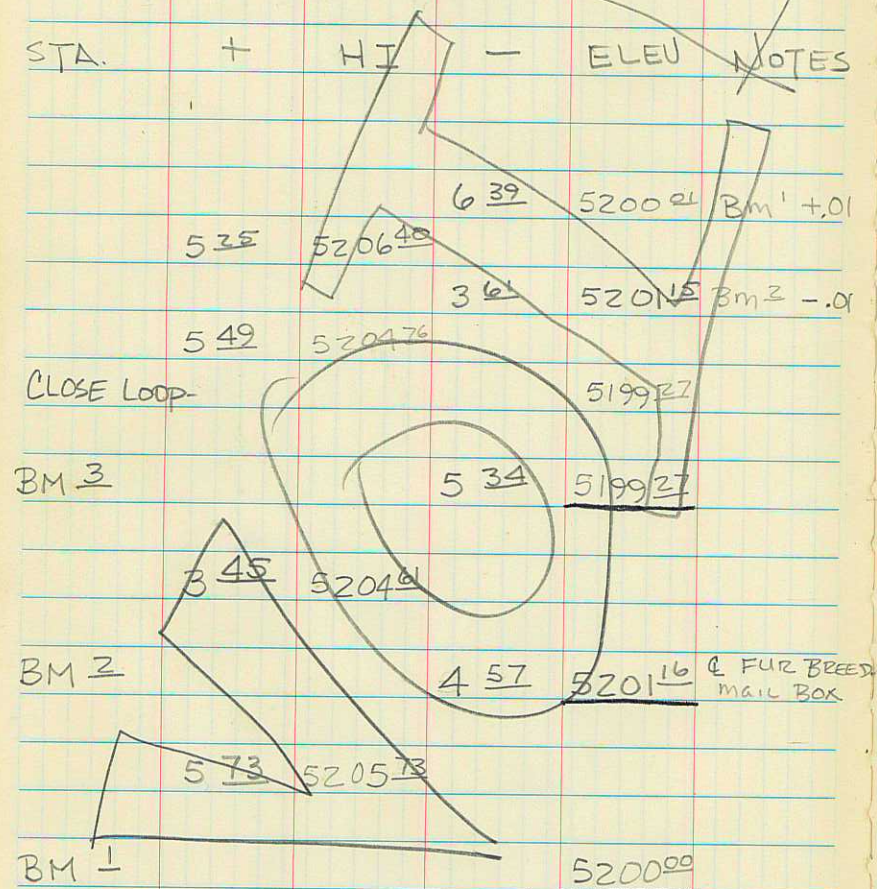
SEPT. 10, 1982

R. LAPPAY ☉

RAINING

P. WARD ✕

STA. + HI - ELEV NOTES



BM ASSUMED 5200.00 PK NAIL IN  
ROAD ☉ AT HUNSAKERS DRIVEWAY



RECHECK LEVELS ON PREVIOUS PAGE

Sept. 13, 1982

overcast cool

45°

✓ M WARD

✓ T LAPRAY

♀ RUSSELL

+ HI - ELEV

6 25 5200 15

5 42 5206 40

3 55 5200 98  
5 42

5 48 5204 53  
3 55

5 48 5199 05  
5 48

3 49 5204 53  
5 48

5 00 5201 04  
3 49

6 04 5206 04

5200 00 5200 00

BM ♀ ASSUMED 5200 00



	+	HI	-	ELEV	
BM#1		5200 <sup>00</sup>			
BM#2		5201 <sup>01</sup>			
BM#3		5199 <sup>06</sup>			
			6 46	5199 <sup>22</sup>	
5 43		5206 <sup>45</sup> <sub>6 40</sub>	3 56	5201 <sup>02</sup> <sub>+ 5 43</sub>	
5 52		5204 <sup>58</sup> <sub>3 50</sub>	5 80	5199 <sup>06</sup> <sub>+ 5 80</sub>	3
3 85		5204 <sup>86</sup> <sub>- 5 80</sub>	5 24	5201 <sup>01</sup> <sub>+ 3 85</sub>	2
6 25		5206 <sup>25</sup> <sub>- 5 24</sub>		5200 <sup>00</sup>	1

### ELEV. OF NORTH PIPE STA 0+00

BM 5200<sup>00</sup>      PIPE # - 1343  
+ 6<sup>12</sup>      # ELEV 5192<sup>69</sup>

HI 5206<sup>12</sup>  
1343  
5192<sup>69</sup>  
343  
520612

### ELEV OF SOUTH BEGIN STA 8+00

BM 5199<sup>06</sup>      DITCH ROD - 874  
+ 5<sup>03</sup>      # EL 5195<sup>35</sup>

HI 5204<sup>09</sup>  
874

### PIPE AT CHURCH PROP. GATE STA 6+75

HI 5204<sup>02</sup>  
SO # ROD - 824      ELEV 5195<sup>15</sup>  
N # ROD - 911      ELEV 5194<sup>28</sup>



LEVEL NET FOR GRADES ON  
 10<sup>TH</sup> WEST DITCH BEGIN STA.  
 BM 3

+	HI	-	ELEV.
			5199. <sup>06</sup> BM 3
5 51	5204 <sup>43</sup>	5 14	
			5199 <sup>52</sup> BM 4
5 84	5205 <sup>34</sup>	4 54	
			5200 <sup>82</sup> BM 5
4 965	5205. <sup>785</sup>	5 01	
			5200. <sup>715</sup> BM 6
5 61	5206. <sup>385</sup>	9 20	
			5196. <sup>685</sup> F.L.
9 21	5206 <sup>395</sup>		
			5 69

FL. OF NORTH END OF RIGGS PIPE  
 (INLET) (MID PT TURN BACK)



	+	HI	-	ELEV
				5200.705 BM 6
5 31		5206.015	5 205	
				5200.81 BM 5
4 52		5205.33	5 81	
				5199.52 BM 4
5 11		5204.63	5 55	
				5199.06 BM 3
			9 41	5195.22 FL. PIPE

### Summary

BM #4	5199.52
BM #5	5200.81
BM #6	5200.71

SOUTH SIDE CHURCH PIPE



LISTING OF BM'S & THEIR  
ELEVATIONS

BM #	ELEV.
BM 1	5200 <sup>00</sup>
BM 2	5201 <sup>01</sup>
BM 3	5199 <sup>06</sup>
BM 4	5199 <sup>52</sup>
BM 5	5200 <sup>81</sup>
BM 6	5200 <sup>71</sup>



+ HI - ELEV

5200.21 BM C

5.44

5206<sup>15</sup>

10<sup>29</sup> 5195<sup>86</sup> OUTLET  
RICKS 2

10<sup>40</sup> 5195<sup>79</sup> INLET  
RICKS 2

10<sup>10</sup> 5196<sup>02</sup> OUTLET  
RICKS 1

9<sup>41</sup> 5196<sup>74</sup> INLET  
RICKS 1

4.94

520081 5.

4.94

5205<sup>75</sup>

9<sup>24</sup>

9<sup>72</sup>

5196<sup>21</sup>

5196<sup>03</sup>

9<sup>63</sup> 5196<sup>12</sup>  
OUTLET  
ROD READ

9<sup>63</sup>  
INLET  
ROD READ

5196<sup>12</sup>

HI 5205 75

5205 75

5196 12

963



STA	+	HI	-	ELEV	DESIGN ELEV
BM				5200.71	
	5.01				
$\pi$		5205.72			

E No				5196.32	
E 50				5196.32	

<del>STA</del>	+	HI	-	ELEV	DESIGN ELEV
B.M.				5200.71	
	5.25				
		5205.96			

E				5196.32	
---	--	--	--	---------	--

BM				5200.71	
	5.27				
		5205.98			

E				5196.32	
---	--	--	--	---------	--

LOD

5205.96
5196.32
<hr/>
9.64

9.37

9.37

5205.98
5196.32
<hr/>
9.66

9.64

9.66

5205.96



STA + HI - BLEU DESIGN  
ELEV.

B.M. 5200.71

T 5.46 5206.17

FL 5196.69

B.M. 5200.71

5.55

5206.26

10.09

5196.17 5196.69

ROD  
5206.17  
5196.69  
9.48

<sup>69</sup>  
9.48  
9.69  
10.35

9.57  
  
9.57

5196.69  
9.57  
5206.26  
  
10.36  
9.57  
.79



prolongation of STA LINE

+	HI	-	ELEV
			5200 <sup>21</sup> BM C
5 <sup>48</sup>			
	5206 <sup>19</sup>		
		9 <sup>14</sup>	
			5197 <sup>05</sup> OUTLET OF HAWKS PIPE
		9 <sup>0</sup>	
			5197 <sup>19</sup> INLET OF HAWKS PIPE
		4 <sup>05</sup>	T.P.
			5201 <sup>54</sup>
6 <sup>16</sup>			
	5207 <sup>20</sup>		
		10 <sup>21</sup>	
			5197 <sup>49</sup> OUTLET
		9 <sup>23</sup>	
			5197 <sup>27</sup> INLET
		6 <sup>16</sup>	
			5201 <sup>54</sup> T.P.
4 <sup>70</sup>			
	5206 <sup>24</sup>		
		5 <sup>51</sup>	
			5200 <sup>73</sup>

STA

STA.  
26+90



STA → STA + H/I - ELEV

BM #6

5.06

5200.71

5205.77

DESIGN ELEV C/E

5196.69

9.08

INLET

5196.58

9.19

OUTLET



11/1/82  
Scott  
Ross

X-DRAIN ELEV.

STA → STA + MI ~~MI~~ ELEV

B.M. #3 5199.06

5.06

π

5204.12

9.50

X DRAIN STA 6+50  
INLET

9.30

X DRAIN STA 6+50  
OUTLET

9.25

100' EAST STA 6+50

4.65

TP STA 9+00 5199.47

4.21

π

5204.13

6.19

X DRAIN STA 13+75  
INLET

STRUCTURE  
ELEV

5194.62 70' LONG 24" CURB

5194.82

5194.87

5197.99



STA → STA + HI - ELEV.

X DRAIN STA 13+75  
OUTLET

7.72

7.80

100' EAST

3.42

T.P. - B.M.

5200.76

4.46

π

5205.43

9.68

X DRAIN STA 16+25  
OUTLET

9.78

X DRAIN STA 16+25  
OUTLET

9.45

100' EAST

3.96

T.P. STA 20+00

5201.46

4.82

π

5206.28

STURTURE  
ELEV.

100' LONG

5196.41

5196.38

5195.74

70' LONG

5195.64

5195.92



STA → STA + HI - ELEV

			8.73	
DRAIN	STA 22450			
	INLET		8.39	
DRAIN	STA 22459			
	OUTLET		7.91	
	100' EAST		5.54	
	B.M.			620074

STRUCTURE  
ELEV.

5197.55	70' LONG
5197.89	
5198.32	



8-22-83

ROSS  $\pi$

JIM  $\rho$

CLEAR.

WARM 75° F

LEVELS TO ESTABLISH GRADE  
FOR NEW DITCH ON EAST  
SIDE OF 10<sup>TH</sup> WEST BETWEEN  
200 NORTH & 200 SOUTH

STA  $\rightarrow$  STA + HI - ELEV.

STA	HI	ELEV.
	3 <sup>00</sup>	5201.01
	5204.01	
0+00	456	5199.45 ✓
1+00	6 <sup>30</sup>	5197.71 ✓
2+00	8 <sup>65</sup>	5195.36 ✓
3+00	8 <sup>29</sup>	5195.72 ✓
4+00	8 <sup>24</sup>	5195.77 ✓

BM # 2 NAIL IN  $\rho$  @ VALLEY METAL

FL OF CANAL BEARING EAST.



STA → STA	+	HI	-	ELEV.
5+00			7 <sup>37</sup>	5196. <sup>64</sup> ✓
6+00			7 <sup>29</sup>	5196. <sup>72</sup> ✓
7+00	T.P.	8 <sup>62</sup>	6 <sup>92</sup>	5197. <sup>09</sup> ✓
		5205. <sup>71</sup>		
8+00			7 <sup>74</sup>	5197. <sup>97</sup> ✓
8+15			7 <sup>47</sup>	5198. <sup>24</sup> ✓
8+36			5 <sup>91</sup>	5199. <sup>80</sup> ✓
9+00			6 <sup>72</sup>	5198. <sup>99</sup> ✓
10+00			7 <sup>19</sup>	5198. <sup>52</sup> ✓
10+30			7 <sup>25</sup>	5198. <sup>46</sup> ✓
<sup>10</sup> 9+30			5 <sup>25</sup>	5200. <sup>46</sup> ✓
<sup>10</sup> 9+30			6 <sup>45</sup>	5199. <sup>06</sup> ✓
<sup>10</sup> 9+30			9 <sup>66</sup>	5196. <sup>05</sup> ✓

FENCE INTERSECTION.

Q OF ROAD BEARS EAST

N EDGE OF DRIVE TO MINE ON E SIDE OF ROAD

CROSS DRAIN POINT

Q OF ASPHALT ROAD 10<sup>TH</sup> WEST

T.B. EAST SIDE OF DITCH ON W SIDE OF 10<sup>TH</sup> WEST

F.L.



STA → STA	+	HI	-	ELEV
<sup>10</sup> 9+30			6 <sup>78</sup>	5198.93
<sup>10</sup> 9+30			10 <sup>78</sup>	5194.93
<sup>10</sup> 9+15			9 <sup>24</sup>	5196.47
11+00			8.19	5197.52 ✓
11+48			8 <sup>80</sup>	5196.91 ✓
12+00			6 <sup>20</sup>	5198.81 ✓
13+00			6 <sup>81</sup>	5198.90 ✓
14+00			6 <sup>49</sup>	5199.22 ✓
14+72	F.P.		6 <sup>25</sup>	5199.46 ✓
		7 <sup>02</sup>		
		5206 <sup>53</sup>		
15+00			8 <sup>51</sup>	5198.02 ✓
16+00			8 <sup>55</sup>	5197.98 ✓

TOP OF BANK WEST SIDE

FL OF DITCH RUNNING WEST \*

FL INLET TO CORBRIDGE DRIVEWAY PIPE

FENCE INTER. EAST.

FENCE INTER. EAST.

TRANSIT @ FENCE INTER.



STA → STA	+	HI	-	ELEV.
17+00			8 <sup>81</sup>	
				5197.72 ✓
18+00			8 <sup>36</sup>	
				5198.17 ✓
18+21			8 <sup>13</sup>	
				5198.40 ✓
19+08			6 <sup>83</sup>	
				5199.20 ✓
20+00			6 <sup>72</sup>	
				5199.81 ✓
21+00			6 <sup>59</sup>	
				5199.94 ✓
21+49			5 <sup>96</sup>	
				5200.51 ✓
TP NE COR			6 <sup>59</sup>	
500. Box				5199.94
	6 <sup>74</sup>			
		5206 <sup>68</sup>		
RETURN. FP.			5 <sup>72</sup>	
				5200.96



FENC INTER. EAST.

R/W LINE 1/2 FT. LOWER.

R/W 1/2 FOOT LOWER.

INTERSECT 200 SOUTH.



STA → STA    +    HI    -    ELEV.

4<sup>64</sup>

5205.<sup>60</sup>

5<sup>89</sup>

5199.71

4<sup>72</sup>

5204.<sup>43</sup>

3<sup>38</sup>

CLOSE ON BM

# 2

5201.05

(0.04 DIFF) [5201.01]



LEVEL NET TO INDICATE  
 ELEVATIONS ON OUTLET  
 OF CORBRIDGE APPROACH C.M.P.  
 & INLET ON C.M.P UNDER  
 200 NORTH STREET (VALLEY  
 VIEW HIGHWAY) @ THE N.E.  
 CORNER OF T. EARL ALLSOP  
 PROPERTY

BENCHMARK # 2 (5201.01 ASSUMED)  
 WAS USED FOR OUR BASIS

STA → STA	+	HI	-	ELEV.
				5201.01
	4	95		
		5205.	46	
		12	73	
				5192.73
		12	37	
				5193.09
		12	37	
				5193.09
		11	42	
				5194.04

*Robert J. Spurr*

9-22-83

FL CMP UNDER 200 N. INLET

FL CMP (ACCESS TO HUNSAKER) INLET

FL CMP (" " " ) OUTLET

FL CMP @ VALLEY METALS OUTLET



STA → STA    +    HI    -    ELEV

				5205. <sup>46</sup>
			11 <sup>26</sup>	
			4 <sup>45</sup>	5194. <sup>20</sup>
				5201 <sup>01</sup>
	3 <sup>01</sup>			
		5204. <sup>02</sup>		
			9. <sup>26</sup>	
			8 <sup>89</sup>	5194. <sup>76</sup>
			9. <sup>75</sup>	5195. <sup>13</sup>
			7 <sup>27</sup>	5194. <sup>27</sup>
	7. <sup>18</sup>			5196. <sup>75</sup>
		5203. <sup>93</sup>		
			2 <sup>92</sup>	
				5201 <sup>01</sup>

F.L. CMP @ VALLY METALS INLET

T.P @ BM # 2

F.L. CMP @ CHURCH PROP OUTLET

F.L. CMP @ " " INLET

F.L. CMP CROSS DRAIN @ CHURCH PROP.

F.L. CMP @ CORBRIDGE PROP OUTLET

T.P. @ OUTLET CORBRIDGE

BM #2 CLOSE!!



9-22-83

WARM 70°

P check BM # 3 w/ BM # 2

STA	STA	+	HI	-	ELEV.
-----	-----	---	----	---	-------

3<sup>73</sup>

5204.<sup>74</sup>

5<sup>68</sup>

5199.<sup>06</sup>

5<sup>10</sup>

5204.<sup>16</sup>

4.<sup>39</sup>

5199

BM # 2

BM # 3



Ross T  
Jim P

11-2-83  
cool 45°

10000 WEST  
WEST SIDE

①

STA	+S	TS	-HI	-S	EL STA	G	CUT	FILL	NOTES
B.M.#2		5 <sup>30</sup>			5201 <sup>01</sup>				
					5206 <sup>31</sup>				
0+00			7 <sup>51</sup>		98. <sup>80</sup>	0+0 93 <sup>75</sup>	5.05	-	INLET +2.37 (1.87)
0+20			8 <sup>26</sup>		98. <sup>05</sup>	0+20 93 <sup>73</sup>	4.32	-	OUTLET +3.10
0+70			7 <sup>72</sup>		98. <sup>59</sup>	0+70 93 <sup>67</sup>	4.92	-	+2.50 (2.00)
1+20			7 <sup>29</sup>		99. <sup>02</sup>	1+20 93. <sup>61</sup>	5.41	-	+2.01
1+70			7 <sup>20</sup>		99. <sup>11</sup>	1+70 93. <sup>55</sup>	5.56	-	+1.86
2+20			6 <sup>80</sup>		99. <sup>51</sup>	2+20 93 <sup>49</sup>	6.02	-	+1.40
2+70			5 <sup>96</sup>		00. <sup>35</sup>	2+70 93 <sup>43</sup>	6.92	-	+0.50
2+80			5 <sup>97</sup>		00. <sup>34</sup>	2+80 93 <sup>42</sup>	6.91	-	+0.51
3+20			6 <sup>31</sup>		00. <sup>00</sup>	3+20 93. <sup>36</sup>	6.64	-	+0.78
3+70			6 <sup>41</sup>		99. <sup>70</sup>	3+70 93 <sup>30</sup>	6.40	-	+1.02
4+20			7 <sup>31</sup>		99. <sup>00</sup>	4+20 93 <sup>24</sup>	5.76	-	+1.66

0.12%



②

STA	+	HI	-	STA EL.
4+70			7 <sup>33</sup>	98. <sup>98</sup>
5+20			7 <sup>47</sup>	98. <sup>84</sup>
5+40			8 <sup>27</sup>	98. <sup>04</sup>
5+60			8 <sup>14</sup>	98. <sup>17</sup>
BM#2			5 <sup>30</sup>	5201. <sup>01</sup>

0.12%  
|  
|  
|  
|

GRADE	CUT	FILL	NOTES
4+70 93 <sup>18</sup>	4.80	-	+1.62
5+20 93 <sup>12</sup>	4.72	-	+1.70
5+40 93 <sup><del>09</del>10</sup>	4.94	-	INLET +2.48
5+60 93 <sup>09</sup>	5.08	-	OUTLET +2.34
CLOSE			



STA. +s HI -s EL STA G.

BM. 4.61 (5205.62) 5201.01

2+80 5.22 5200.40 5193.42

3+20 5.52 5200.01 5193.36

~~BM.~~ 4.50 (5205.51) 5201.01

2+80 5193.42

3+20 5193.36

BM 5201.01

3.68

(5204.69)

10.96

5193.73

10.94

5193.75

CUT FILL R. ROD

12.20

12.26

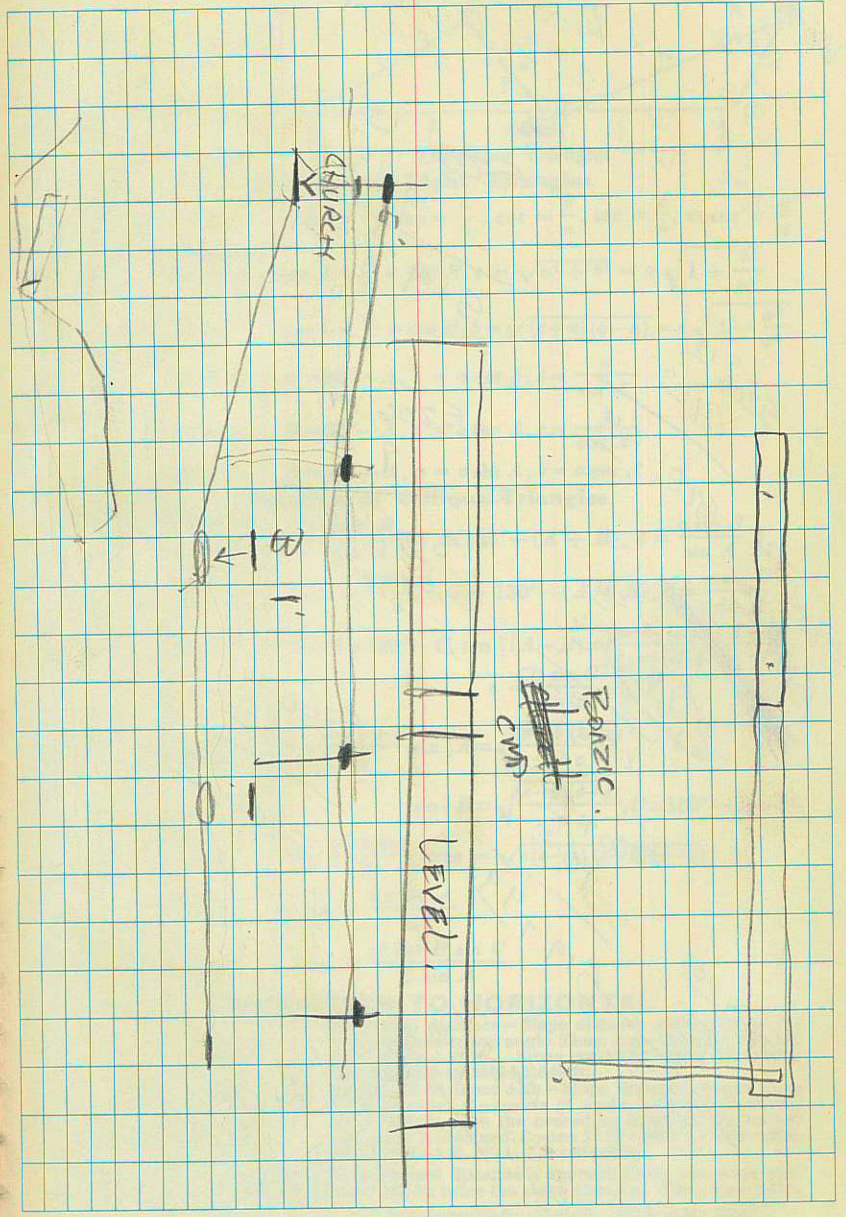
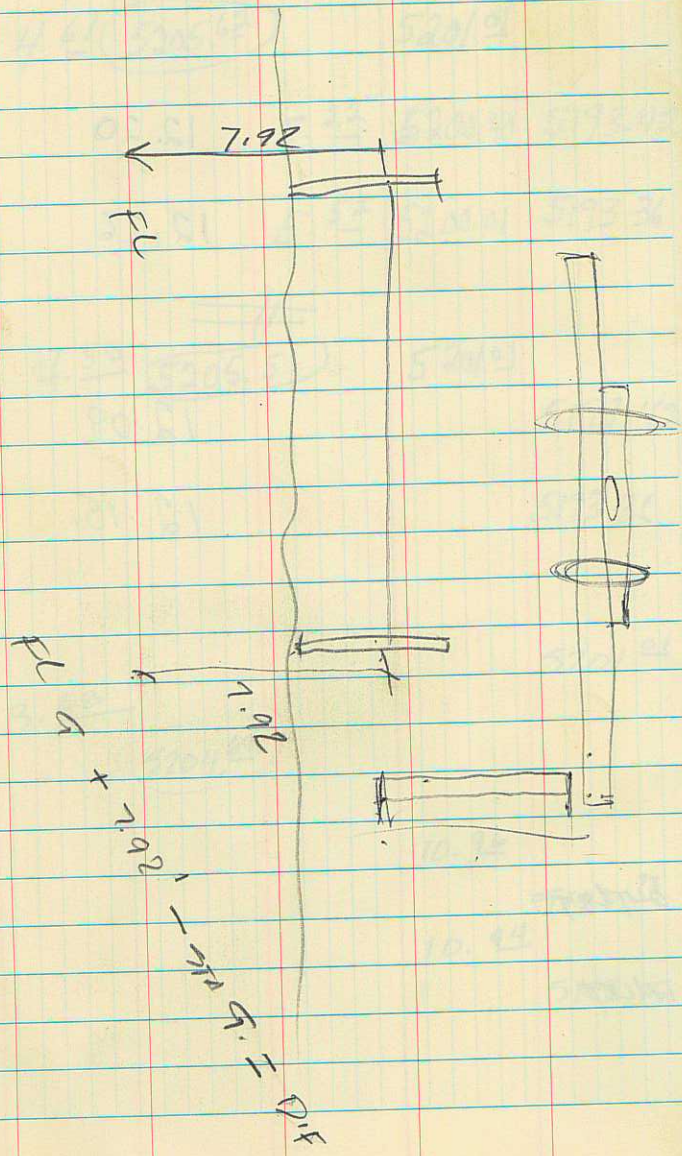
12.09

12.15

OUTLET

INLET







WESTBND  
 62. to CAROL 10. wide  
 292. to RIVER  
 27. TO N 25 WIDE  
 103. TO N 80 E LONG. WIDE

5206<sup>19</sup>  
 9.14  
 5197.09

5206<sup>19</sup>  
 4.39  
 5201.54

5204<sup>24</sup>  
 5199.00  
 5201.44  
 5207.20

5206<sup>24</sup>  
 5.91  
 5200.73

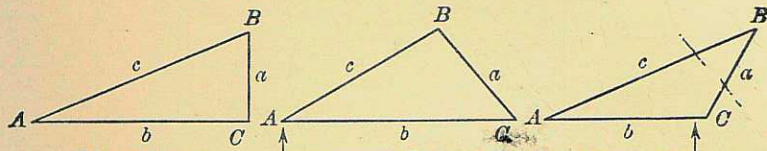
5207<sup>20</sup>  
 10.21  
 5197.49

5207<sup>20</sup>  
 9.73  
 5197.91

5207<sup>20</sup>  
 6.16  
 5201.54

5206<sup>24</sup>  
 4.70  
 5206.24

### TRIGONOMETRIC FORMULAS



Right Triangle  
 Oblique Triangles

**Solution of Right Triangles**

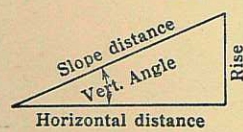
For Angle A.  $\sin = \frac{a}{c}$ ,  $\cos = \frac{b}{c}$ ,  $\tan = \frac{a}{b}$ ,  $\cot = \frac{b}{a}$ ,  $\sec = \frac{c}{b}$ ,  $\text{cosec} = \frac{c}{a}$

Given	Required	Formulas
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B$ , $c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B$ , $b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A$ , $b = a \cot A$ , $c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A$ , $a = b \tan A$ , $c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A$ , $a = c \sin A$ , $b = c \cos A$

**Solution of Oblique Triangles**

Given	Required	Formulas
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}$ , $C = 180^\circ - (A + B)$ , $c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}$ , $C = 180^\circ - (A + B)$ , $c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C$ , $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$ $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}$ , $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$ $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$ , $C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}$ , $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

### REDUCTION TO HORIZONTAL



Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle =  $5^\circ 10'$ . Since  $\cos 5^\circ 10' = .9959$ , horizontal distance =  $319.4 \times .9959 = 318.09$  ft.  
 Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained.  $\text{Cosine } 5^\circ 10' = .9959$ .  $1 - .9959 = .0041$ .  $319.4 \times .0041 = 1.31$ .  $319.4 - 1.31 = 318.09$  ft.

When the rise is known, the horizontal distance is approximately the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft., slope distance = 302.6 ft. Horizontal distance =  $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$  ft.